Velian's reputation as the designer and manufacturer of fluid power products of utmost reliable quality is an established fact for over 45 years now.
With the back-up of up-to-date \& state-of-the-art production facilifies and a clear-cut focus on design engineering and product development, Velian effectively meets the demand for a very wide spectrum of applications, such as in :

- MACHINE TOOLS
- MOBILE MACHINERY
- MARINE EQUIPMENT
- STEEL MILL EQUIPMENT
- PACKAGING MACHINERY
- CONSTRUCTION MACHINERY
- MINING EQUIPMENT
- POWER PROJECTS EQUIPMENT
- STABILISERS AND STEERING GEARS
- FORGE AND FOUNDRY EQUIPMENT
- PLASTIC MACHINERY
- AMUSEMENT PARKS, ETC.

Besides hydraulic and pneumatic cyl inders for every conceivable application, Velian continues to engineer, manufacture and market a wide range of preumatic producits.
To achieve, maintain and provide a "single source system" facility, Velian's joint venture company manufactures high performance Hydraulic Pumps, Motors, Valves and Systems. This has enabled Velian products and services to be reckoned as the benchmarks for quality.

While this catalogue is intended as a brief guide to the selection of standard Velian Hydraulic Cylinders, Velian also offers customised equipment and the specials needed by its valued and satisfied customers drawn from varie us sectors of the industry who have been regularly sourcing their requirements of these cylinders and other fluid power products from Velian.

Velian, with its proven trackrecord, technical expertise, design and engineering capabilities in the realm of high quality products and prompt services is confident of satisfying the exacting demands of all its customers.

Veljan offers various types of Hydraulic Cylinders for different pressure ratings and applications:

## Series-HT

Compact tie-rod square type construction Hydraulic Cylinders rated for 160 bar with mounting dimensions conforming to $I S O: 6020$ part 2 for 40 to 200 mm bore and ISO:6020 part 3 for 250 and 320 mm bore sizes.


## Series-HR

Non-tie-rod welded round type construction of 160 bar medium series Hydraulic Cylinders with mounting dimensions conforming to ISO:6020 - part 1, in bore sizes from 40 to 320 mm .
The above HT and HR series cylinders are also suitable for use at working pressures upto 210 bar depending on the rod-end and mounting considerations.

## Series-HH

Heavy duty Hydraulic Cylinders rated for 250 bar pressure with mounting dimensions conforming to ISO:6022, in bore sizes from 50 to 320 mm .


## Specials

Special Cylinders such as duplex, tandem, telescopic and other custom-designed types are regularly produced for various applications and pressures upto 500 bar and bores upto 800 mm dia.
Velian also manufactures a wide range of pneumatic cylinders rated for pressures upto 17 bar in bore sizes ranging from 8 to 800 mm .

## Veljan offers the following variety of seals to suit different applications:

## PISTON SEALS

ELASTOMERIC Piston seals with integral anti-extrusion Rings are fitted as a standard for 160 bar application. Compact seals with bearing rings conforming to ISO:6547 dimensions and leak-tight under normal operating conditions are optional. These are suitable for speeds upto $0.5 \mathrm{~m} / \mathrm{s}$ and holding loads in position.

LOW FRICTION Piston Seals conforming to ISO:7425-1 grooves employ an elastomer energised PTFE ring and may be used for piston speed upto $5 \mathrm{~m} / \mathrm{s}$. These are best suited where very low friction and an absence of stick-slip are needed, such as in Servo cylinders. These permit fine control of position, velocity and acceleration. However they are not suitable for load holding applications.

SPRING LOADED PTFE U-CUPS are suitable for low as well as high temperatures. For maximum dynamic sealing and to prevent turning or rolling, these seals are mechnically locked in place and pressed against tubing ID.

CAST IRON PISTON RINGS bffer exceptional durability and are recommended for high temperature application. Leakage inherent in this design can result lin slip, drift and varying feed rates and hence are not suitable for holding loads in position.

## ROD SEALS

POLYURETHANE internally lubricated Rod Seals with hardness of $90^{\circ}$ Shore $A$, are compatible with a broad range of temperature and fluids. They have low compression set and excellent abrasion resistance. They are designed to install easily and function well in normal applications and are fitted as standard. Rod seals conforming to ISO 5597 are optional.

LOW FRICTION Rod Seals to suit ISO:7425-2 grooves, employ an elastomer energised PTFE ring and may be used for piston speeds upto $5 \mathrm{~m} / \mathrm{s}$. These are used in conjunction with similar Piston Seals indicated alongside.

PTFERod Seals are pressure-energized and wear compensating, mechanically locked to prevent blowout and will endure temperatures upto $230^{\circ}$ F. They are compatible with most hydraulic fluids including fire-resistant types.

ROD WIPER protects the Rod Seal and bush from damage caused by dirt adhering to the rod. The lip of the wiper removes the finest dirt from the piston rod.

ROD WIPER

The following simple steps ensure that principal factors are considered while selecting the cylinder :

1. First Establish:
-Force (F) needed or weight to be moved
-Stroke or distance to be travelled.
2. Based on the available or selected system pressure P , calculate the cylinder areas required by using the formula $\mathrm{F}=\mathrm{P}$ A for push as well as pull applications.
3. Referring to the table below, choose the minimum bore \& rod combination to provide calculated areas.

AREAS IN DIFFERENT BORE ROD COMBINATION

| Bore <br> mm | Cap end area for push $\mathrm{cm}^{2}$ | Rod <br> dia <br> mm | Head end area for Pull $\mathrm{cm}^{2}$ | $\begin{gathered} \hline \text { Bore } \\ \mathrm{mm} \end{gathered}$ | Cap end area for Push $\mathrm{cm}^{2}$ | $\begin{array}{\|l\|} \hline \text { Rod } \\ \text { dia } \\ \mathrm{mm} \\ \hline \end{array}$ | Headend area for Pull cm² |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 40 | 12.57 | 18 | 10.02 | 125 | 122.72 | 56 | 98.09 |
|  |  | 22 | 08.77 |  |  | 70 | 84. 23 |
|  |  | 28 | 06.41 |  |  | 90 | 59. 10 |
| 50 | 19.63 | 22 | 15.83 | 160 | 201.06 | 70 | 162. 58 |
|  |  | 28 | 13.48 |  |  | 90 | 137. 44 |
|  |  | 36 | 09.46 |  |  | 110 | 106,03 |
| 63 | 31.17 | 28 | 25.02 | 200 | 314.16 | 90 | 250. 54 |
|  |  | 36 | 21.00 |  |  | 110 | 219. 13 |
|  |  | 45 | 15.27 |  |  | 140 | 160.22 |
| 80 | 50.27 | 36 | 40.09 | 250 |  | 140 | 336.94 |
|  |  | 45 | 34.36 |  |  | 60 | 289. 81 |
|  |  | 56 | 25.64 |  |  |  | 236. 40 |
| 100 | 78.54 | 45 | 62.64 | 320 | 804.25 | 180 | 549. 78 |
|  |  | 56 | 53.91 |  |  | 200 | 490. 09 |
|  |  | 70 | 40.06 |  |  | 220 | 424. 12 |

4. Check the rod diameter for column strength to resist push force in case of long stroke cylinders (refer page 14), and also the speed ratio between the return and forward strokes, etc.
5. Select the mounting style and the rod end/ cap end accessories to fit your installation needs. (refer pages 20 to 33)
6. Application considerations may require changes in your selection, and for assistance refer the following Application Engineering section.

APPLICATION ENGINEERING

| Application | Check the following |
| :--- | :--- |
| Acceleration <br> and <br> DecelarationCheck whether the calculated <br> force is sufficient to accelerate/ <br> decelerate the load within prescribed <br> distance. Check back-pressure rise <br> during cushioning is within limits. |  |
| Piston speed | Check whether the standard port size <br> permits sufficient oil flow to meet <br> speed requirements. |
| Long stroke <br> horizontal <br> mounting | Check whether a stop tube is needed <br> to prevent excess bearing load <br> \& wear. |
| High column <br> loading | Check whether standard piston <br> rod is strong enough in buckling. |
| High or low <br> temperature | Below Oo Cor above 800 C, spring <br> loaded PJFE/ Viton seals are to be <br> opted. For very high temperature, <br> piston rings can be used if leakage <br> is permitted. |
| Non-petroleum <br> based fluids |  |
| PTFE seals are compatible with most <br> fire-resistant and petroleum-based <br> fluids. Ohter seals are available for <br> high water base and other fluids. |  |

VARIATIONS FROM STANDARD

1. Ports : BSP ports are standard. Other types like BSPT, NPT, `O' ring seal ports, SAE flanged ports, manifold ports, etc., can be optionally provided. Also refer 'Piston speed' on Page 15.
2. Cushion Adjustments : Ball check and adjusting screws can be interchanged without affecting port locations.
3. Mixed mounting for special or constrained installations.
4. Heavy chrome plated or stainless steel piston rods for corrosive environments.
5. Longer rod extensions as desired.
6. Rod-end threads : Shouldered male threads in metric sizes are standard as listed in the basic cylinder dimensions table. These threads have turndown of approximately $50 \%$ of the Piston rod area. The screwing of the mating part is done upto the shoulder, eliminating the need for locknut. Two variations are possible as follows:
(i) Female threads of same size as indicated above - these are useful for connecting mating parts such as rod-eyes having male threads.
(ii) Unshouldered male threads, i.e threads of full diameter as that of rod, useful when adjustment is needed, along with a locknut for locking the attachment.

It is often necessary to determine the Force $F$ required to accelerate or decelerate a given mass. The maximum velocity ' $V$ ' attained by a mass ' $m$ ' over a distance ' $s$ ' is dependant on the force ' $F$ ' related as follows: $F=m a$ where $a=\frac{v^{2}}{2 s}$
These forces will help in selecting a proper size cylinder, pump pressure etc. They will also help in checking the safety of various system components by finding out the pressure rise when a moving load is stopped by means of internal cushions. The following examples well help in understanding these. Care should be taken to consider friction in actual applications, since this is neglected here. The frictional force is to be added while determining the acceleration force and subtracted for deceleration force.
EXAMPLE 1: Vertical motion.
For Acceleration downward or Deceleration upward: $F=m(a-g)$.
For Acceleration upward or Deceleration downward: $F=m(a+g)$.
$V=15 \mathrm{~m} / \mathrm{min}$ moving down, $m=5000 \mathrm{~kg}, \mathrm{~s}=12 \mathrm{~mm}$
Acceleration, $a=\frac{(15 / 60)^{2}}{2 \times 0.012}=2.604 \mathrm{~m} / \mathrm{sec}^{2}$
$F=\frac{5000(2.604-9.81)}{9.81}=-3672 \mathrm{kgf}$
The negative sign indicates gravity alone is sufficient to cause acceleration.
EXAMPLE 2: Horizontal motion $\mathrm{F}=\mathrm{ma}$
Let us consider the same values as above. As acceleration foree of 5000 * $2.604 / 9.81=1327 \mathrm{kgf}$ is required to move a mass of 5000 kgs over a distance of 12 mm with a max. velocity of $15 \mathrm{~m} / \mathrm{min}$.

Assume 160 bar pump is available.
The area of cylinder required $=$ force / pressure $=\frac{1327}{160}=8.294 \mathrm{~cm}^{2}$ which corresponds to a bore of 32.5 mm . The next higher standard 40 mm bore and 18 mm rod cylinder (cap end area $=12.57 \mathrm{~cm}^{2}$ and head end area $\left.=10.02 \mathrm{em}^{2}\right)$ with pressure rating of 160 bar seems to be sufficient.

There is another factor to be checked - i.e. whether the deceleration forces set up by cushioning inside the cylinder cause any harm to it. Hence it should be determined (1) whether the cylinder is required to stop the mechanism, (2) or whether the mechanism stops the cylinder. The second case is not harmful but in the first case, we have to check whether the back pressure created inside the cylinder is well within the safe limit. To determine this, we shall assume the above weight is to be decelerated over a distance of 16 mm for a horizontal motion.

Deceleration rate $=\frac{(15 / 60)^{2}}{2 \times 0.012}=1.953 \mathrm{~m} / \mathrm{sec}^{2}, \quad$ Deceleration force $=\frac{5000 \times 1.953}{9.81}=-995.5 \mathrm{kgf}$
Total force to be created on rod side $=995.5+1327=2322.5 \mathrm{kgf}$
Back pressure created in the cylinder $=\frac{2322.5}{10.02}=231.8 \mathrm{kgf} / \mathrm{cm}^{2}$
Thus the back pressure exceeds the pressure rating. Hence the next larger bore ie. 50 bore and 22 dia rod cylinder with head end area of $15.83 \mathrm{~cm}^{2}$ which gives a back pressure of $146.71 \mathrm{kgf} / \mathrm{cm}^{2}$ is recommended.

In power cylinders, cushioning means deceleration of moving masses. Cushioning extends cylinder life and reduces undesirable noise and hydraulic shock.

1. When Cushions are required.

Cushioned cylinders should be used whenever the piston is required to move heavy loads or travel at high speeds, say more than $0.1 \mathrm{~m} / \mathrm{sec}$. Under both these conditions, the piston will pound the head and cap causing heavy damage to the piston and also heavy deceleration forces will be set up on the moving members. To minimise these effects, a back pressure or resisting force must be built up inside the cylinder to bring the piston to a safe and smooth stop during the last portion of its stroke. Cushions built into the cylinder perform exactly this function.

The ability of cylinder to decelerate and stop inertia loads is dependent on : (a) the volume of cushion chamber which is proportional to the length of cushion stroke for a given size of cylinder; (b) pressure developed in cushion chamber; (c) the efficiency with which the fluid is metered.
For normal applications, standard length cushions are sufficient. Where extremely fast moving loads are involved, special cushions are to be devised to bring load to a stop without bounce.

## 2. When Cushions are not required.

Cushions need not be specified (a) when light loads are moving at low speeds; (b) when external stops are provided thus eliminating the possibility of piston striking the cylinder head and cap; (c) for short stroke ( 50 mm or less) cylinders, because the short stroke does not allow piston speed to build up enough to sufficiently offset the back pressure built up by the cushion.
3. How Cushioning is achieved.


Fig. 1: As the cushion plunger (1) enters the cushion cavity (2) the exhaust fluid is trapped creating back pressure against piston assembly. This back pressure decelerates the movement of piston thus reducing pounding of the piston against head or cap. The degree of cushioning can be obtained as desired by adjusting the screw (4).


FIGURE 2 : CUSHION OUT
Fig. 2 : When fluid under pressure enters the cylinder head end to move the piston in the opposite direction the fluid moves the Ball check (3) off its seat, opening the passage for more pressure fluid to act against the piston, thus speeding its start-up movement as the cushion plunger (1) is immediately forced out of the cavity (2).

From the above illustrations, the cushioning of a cylinder is obtained by trapping the exhaust fluid as the piston assembly nears the end of its stroke. The cushion capacity of the head end is less than that of the cap end and reduces to zero at high drive pressures owing to the pressure intensification across the piston. The energy absorption capacity of the cushion decreases with drive pressure which, in normal circuits, is the relief setting.

## AIR BLEEDS

Hydraulic cylinders vertically mounted or horizontally mounted with ports on top are self bleeding when cycled full stroke and do not require air bleeds. When required or called for, bleed screws can be optionally provided at either end of the cylinder. Location of bleed screws must be specified to suit the accessibility in a particular application. The bleeder port of $1 / 4$ " BSP is standardized for cylinders of 50 mm bore and above. $1 / 8$ " BSP is provided for 40 mm bore cylinders. Minimess type bleed screws are optional.

## GLAND DRAIN

In certain situations like long stroke or high speed operation or cylinders provided with Low Friction rod seal, there is a possibility of oil accumulation in the cavity between the rod seal and wiper. A drain port is provided between the rod seal and wiper seal to evacuate the accumulated oil to the tank of the hydraulic system.

## STROKE ADJUSTMENT

Where absolute precision is required in end position, a screwed adjustable stop can be provided. The illustrations alongside show designs suitable for closed position adjustment and for open position adjustment. It may be noted from the figure that for the open position adjustment, one has to go in for a double rod cylinder.

## SINGLE ACTING CYLINDERS

Normally double acting cylinders are supplied as standard and they can be used as single acting by applying pressure to one side of the piston. The piston will return to its initial position by means of external force or gravity when the applied pressure is removed. For cylinder designs with internally arranged springs, consult Velian.

## MULTIPLE STROKE CYLINDERS

Where definite intermediate stoppings of the piston are required, Veljan offers different designs. One such design with two positions for the piston is shown here.

AIR BLEEDS


STANDARD TYPE


MINIMESS TYPE

## GLAND DRAIN

DRAIN PORT

STROKE ADJUSTMENT


FOR CLOSED POSITION


FOR OPEN POSITION

SINGLE ACTING CYLINDERS WITH SPRING RETURN


MULTIPLE STROKE CYLINDERS


Stop tube is ideal for preventing excessive bearing wear and rod buckling on long push stroke cylinders.

A stop tube is a tubular spacer positioned between the piston and the cylinder head in the extended condition. The increased distance between the piston and the Rod bushing reduces bearing reactions. Stop tubes are useful to prevent buckling of horizontally mounted, long stroke cylinders on push stroke. These are more effective, less costly, and lighter in weight than oversize piston rods.

When to specify stop tubing for your cylinder.
The following simple steps give you the answer :
Step 1: Determine if your cylinder corresponds to any of those illustrated in group A, B or C.

Step 2: If your cylinder is in group $A$, then stop tube is not required but an oversize-rod may be required (see page 14). If your cylinder is in Group B, a stop tube is recommended as given in step 3 below.
If your cylinder is in group $C$, calculate the furning movements and loads between piston and rod bushing. Weight offluid must be included on large bore and/or long stroke cylinders. Determine stop tube length so that load at piston rod bearing does not exceed 15 kgs for each square cm . of bearing area. Also check for stop tube length as given in step 3 below and use the longer of the two stop tubes calculated.

Step 3: Determine the value of "LD" from instructions in Group B/C. Be sure to include thickness of cylinder head, cap and piston assembly plus $2 \times$ cylinder stroke. If the value of "L" is more than 1000 mm , then 10 mm long stop tube is recommended for each 100 mm of " "" beyond 1000 mm .

Step 4: Add stop tube length to your original " $\lfloor$ " dimension to obtain your adjusted "L" dimension.

For example, consider a situation with "L" $=1800 \mathrm{~mm} . \&$
Stop tube $=80 \mathrm{~mm}$ Adjusted "L" $=1800+80 \mathrm{~mm}=1880 \mathrm{~mm}$
From the illustrations, it is clear that for a given size of cylinder, a pivot mounted arrangement requires longer stop tube compared to the fixed mounting. In specifying a cylinder with a stop tube, please state the net stroke and the length of stop tube. The addition of the two dimensions will be the gross stroke of the cylinder, which shall be used for arriving at the overall dimension.


Special considerations like piston rod sag in long stroke cylinders, or column strength in long PUSH stroke applications, or speed of piston retraction require oversize piston rods.
It may be noted with caution that higher rigidity of oversize rods will not obsorb side loads, whereas greater flexibility of the smaller standard diameter rod transmits less of the undesirable side loading back to the piston rod bushing.
To determine oversize rod diameter required for PUSH stroke application, follow these simple steps :
STEP 1. Referring to groups $A$ to $C$ of the previous section, determine the value of "l" for your cylinder or use the adjusted value of "L" dimension calculated from step 4 of that section.
STEP 2. From your cylinder bore size and maximum operating pressure, calculate PUSH force $=$ pressure $\times$ area.
STEP 3. In the table below, find your PUSH force in the left column and locate your "L"
dimension or your adjusted value of """ dimension in the same horizontal line to the right lif your exact "L" or adjusted value of "L" dimension is not shown, move to the right to the next larger number). Read vertically up from this number to the rod diameter shown This is the recommended rod diameter for your application.

VALUES OF "L" FOR DIFFERENT FORCE \& ROD SIZE COMBINATIONS:

| Value of Fin Kgf in this column | PISTON ROD DIAMETERS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 18 | 22 | 28 | 36 | 45 | 56 | 63 | 70 | 80 | 90 | 110 | 125 | 140 | 180 | 220 |
| 250 | 1033 | 1544 | 2500 | 4134 |  |  |  |  |  |  |  |  |  |  |  |
| 500 | 731 | 1092 | 1768 | 2923 | 4567 | 7073 | 8952 |  |  |  |  |  |  |  |  |
| 750 | 596 | 891 | 1444 | 2387 | 1391 | 5775 | 7310 | 9023 |  |  |  |  |  |  |  |
| 1000 | 517 | 772 | 1250 | 2067 | 3229 | 5001 | 6330 | 7815 |  |  |  |  |  |  |  |
| 2500 | 327 | 488 | 791 | 1307 | 2042 | 3163 | 4003 | 4942 | 6455 | 8170 |  |  |  |  |  |
| 5000 | 231 | 345 | 559 | 924 | 1444 | 2236 | 2831 | 3495 | 4565 | 5777 | 8630 |  |  |  |  |
| 7500 |  | 282 | 456 | 754 | 1179 | 1826 | 2311 | 2853 | 3727 | 4717 | 7046 | 9100 |  |  |  |
| 10000 |  |  | 395 | 653 | 1021 | 1582 | 2002 | 2471 | 3228 | 4085 | 6102 | 7880 | 9885 |  |  |
| 12500 |  |  |  | 584 | 913 | 1414 | 1790 | 2210 | 2887 | 3654 | 5458 | 7048 | 8841 |  |  |
| 1500 |  |  |  | 533 | 834 | 1291 | 1634 | 2018 | 2635 | 3335 | 4982 | 6434 | 8071 | 13341 |  |
| 20000 |  |  |  | 462 | 722 | 1118 | 1415 | 1747 | 2282 | 2888 | 4315 | 5572 | 6990 | 11554 |  |
| 25000 |  |  |  |  | 646 | 1000 | 1266 | 1563 | 2041 | 2584 | 3860 | 4984 | 6252 | 10334 |  |
| 30000 |  |  |  |  | 590 | 913 | 1156 | 1428 | 1863 | 2358 | 3523 | 4550 | 5707 | 9434 | 14093 |
| 35000 |  |  |  |  | 545 | 845 | 1070 | 1321 | 1725 | 2184 | 3262 | 4212 | 5283 | 8734 | 13047 |
| 40000 |  | , |  |  |  | 791 | 1000 | 1235 | 1614 | 2042 | 3051 | 3940 | 4942 | 8170 | 12205 |
| 50000 |  |  |  |  |  | 707 | 895 | 1105 | 1442 | 1823 | 2729 | 3524 | 4420 | 7307 | 10916 |
| 75000 |  |  |  |  |  |  |  | 902 | 1178 | 1492 | 2228 | 2877 | 3609 | 5966 | 8913 |
| 100000 |  |  |  |  |  |  |  |  | 1020 | 1291 | 1930 | 2492 | 3126 | 5167 | 7719 |
| 150000 |  |  |  |  |  |  |  |  |  |  | 1576 | 2034 | 2552 | 4219 | 6302 |
| 200000 |  |  |  |  |  |  |  |  |  |  |  | 1762 | 2210 | 3653 | 5458 |
| 250000 |  |  |  |  |  |  |  |  |  |  |  | 1576 | 1977 | 3268 | 4882 |

Notes: The above table is prepared using "Euler" formula for bucking and a factor of safery of 4 . For values of "L" less than those shown, the slenderness ratio (length/radius of gyration) is less than 50. Thus the compressive strength formula is to be used rather than the column strength formula on which this table is based. For very low slenderness ratios (below 20), compressive strength formula with factor of safety of 2 is satisfactory. For slenderness ratios between 20 and 50 , use compressive strength formula with proportionate factors of safety between 2 and 5 .

The operating speed of the piston in a hydraulic cylinder depends on fluid flow rate in the connecting pipe lines. The flow is generally expressed in liters per minute, introduced to or expelled from the cap end port. Fluid velocity in connection lines is normally limited to 5 metres per second to minimize fluid turbulence and pressure loss.

The table below gives piston speed in metres per minute, for standard and oversize ports, when the velocity of fluid flow in standard weight pipe is 5 metres per second. If the piston velocity is greater than the tabulated value, then consider the use of larger pipes up to cylinder port, with two ports per cap connected to provide the fluid flow required. Alternatively specify the oversize ports listed in the table. Special over size thickness cap will be required in such a case.

| Cyl. Bore in mm | Catalog standard port |  |  | Oversize Port (optional) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Port } \\ & \text { size } \\ & \text { (BSP) } \\ & \text { inch } \end{aligned}$ |  | Piston speed $\mathrm{m} / \mathrm{min}$ | $\begin{aligned} & \text { Port } \\ & \text { size } \\ & \text { (BSP) } \\ & \text { inch } \\ & \hline \end{aligned}$ |  | Piston speed m/min |
| $\begin{aligned} & 40 \\ & 50 \end{aligned}$ | $\begin{aligned} & 1 / 2 \\ & 1 / 2 \end{aligned}$ | $\begin{aligned} & 40 \\ & 40 \end{aligned}$ | $\begin{aligned} & 31.8 \\ & 20.4 \end{aligned}$ | $\begin{aligned} & 3 / 4 \\ & 3 / 4 \end{aligned}$ |  | $\begin{aligned} & 427 \\ & 27.0 \end{aligned}$ |
| $\begin{aligned} & 63 \\ & 80 \end{aligned}$ | $\begin{aligned} & 3 / 4 \\ & 3 / 4 \end{aligned}$ | $\begin{aligned} & 53 \\ & 53 \end{aligned}$ | $\begin{aligned} & 16.8 \\ & 10.8 \\ & \hline \end{aligned}$ |  | 85 | $\begin{aligned} & 26.7 \\ & 17.0 \\ & \hline \end{aligned}$ |
| $\begin{aligned} & 100 \\ & 125 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 85 \\ & 85 \\ & \hline \end{aligned}$ | $\begin{array}{r} 10.8 \\ 7.2 \\ \hline \end{array}$ | $\begin{array}{r} 11 / 4 \\ \times 1 / 4 \\ \hline \end{array}$ | $\begin{aligned} & 136 \\ & 136 \end{aligned}$ | $\begin{aligned} & 17.3 \\ & 11.1 \end{aligned}$ |
| $\begin{aligned} & 160 \\ & 200 \end{aligned}$ | $\begin{aligned} & 11 / 4 \\ & 11 / 4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 136 \\ & 136 \end{aligned}$ | $\begin{aligned} & 6.8 \\ & 4.3 \end{aligned}$ | $\begin{aligned} & 11 / 2 \\ & 11 / 2 \end{aligned}$ | $\begin{aligned} & 212 \\ & 212 \end{aligned}$ | $\begin{array}{r} 10.5 \\ 6.7 \end{array}$ |
| $\begin{aligned} & 250 \\ & 320 \end{aligned}$ | 11/8 | $\begin{array}{\|l\|} \hline 212 \\ 212 \end{array}$ | $\begin{aligned} & 4.3 \\ & 2.6 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 305 \\ & 305 \end{aligned}$ | $\begin{aligned} & 6.2 \\ & 3.8 \end{aligned}$ |

To suit your requirements, Cylinders can be mounted in a variety of ways and the selection of correct mounting is an important factor for optimum working. The different mounting arrangements used in Fluid Power Cylinders are indicated by Style Nos. consisting of two alphabets followed by one numeral as referred in the text and table alongside.
Cylinder mountings are broadly classified as Fixed mountings-where the end point moves in a straight line and Pivot mountings - where the end point moves in an arc.

Fixed Mountings : These mountings are rigid, strong and provide good support. Fixed mountings can be subdivided as (a) centre-line mountings and (b) off-centre mountings.

Centre-Line Mountings : All Flange mountings (ME5, ME6, MF1, MF2, MF3, MF4, MF5, MF6) Extended tie rod mountings (MX1, MX2, MX3) fall into this category. These mountings keep fixing bolts either in simple tension or shear without principal stress and tolerate misalignment to some extent However, they cannot tolerate constant misalignment and in such case, introduce side loads on bearings. For long stroke cylinders, combination of fixed mountings can be used such as front flange and also foot lugs at the back. Front flange mounting is ideal for tensile load whereas rear flange is ideal for compression loads. Tie rod mountings though require least mounting space are less strongerthan the flange mountings.
Off-Centre Mountings: Foot or side-lug mounting (MS2) and side-tapped or side flush mounting (MS4) come under this category. These are used where cylinders are to be mounted onto surfaces, parallel to axis of cylinders. These mountings try to sway or bend under heavy loads and as such subject the cylinders and also the mounting to principal stress. One method of eliminating this problem is the use of shear keys or dowel pins so that bolts are relieved of compound stresses. Cylinders with integral key, not only takes shear loads but also provides accurate alignment of the cylinder and simplified installation. In case of tensile loads, location of key should be at head-end plate and in case of compressive load, the key should be at the cap-end plate. Only one shear key is to be put either on cap end or head end but not at both ends. This accommodates cylinder strain under pressure and temperature variations.

Pivot Mountings: In this type of mountings, the cylinder body swings in a plane perpendicular to the pivot axis. These are further divided as follows depending on the pivot location:

Clevis/Eye Mountings: (MP1, MP3, MP5) : Here the pivot goes outside the body of the cylinder. Its advantage is felt in using cylinders in linkage mechanisms. MP1 and MP3 mounting tolerate misalignments in one plane. If misalignment is anticipated in all planes, then spherical bearings are to be used at the ends of the cylinders as shown in MP5 mounting.
Trunnion Mountings: (MT1, MT2, MT4): Trunnion support can be at the head end, cap end or at any intermediate position, However, in long stroke cylinders, head end trunnion is recommended so that small size piston rod can be used. Trunnion pins are designed to be under shear load and hence they should not be supported on spherical bearings, as they introduce principal stresses.
The mounting styles covered in different dimensional standards is indicated by K in the table below.

| Mounting StylearrangementNo. |  | ISO : 6020 |  |  | $\begin{aligned} & \text { ISO: } \\ & 6022 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Part 1 | Part2 | Part3 |  |
| Head Rectangular | ME 5 |  | Y |  |  |
| Cap Rectangular | ME 6 |  | Y |  |  |
| Rectangular Flange, Head | MF 1 | Y |  |  |  |
| Reclangular Flange, Cap | MF 2 | Y |  |  |  |
| Circular Flange, Head | MF 3 | Y |  |  | Y |
| Circular Flange, Cap | MF 4 | Y |  |  | Y |
| Square Flange, Head | MF 5 |  |  |  |  |
| Square Flange, Cap | MF 6 |  |  |  |  |
| Fixed Clevis, Head | MP 1 |  | Y | Y |  |
| Fixed Eye, Cap | MP 3 | Y | Y | Y | Y |
| Fixed Eye with Spherical |  |  |  |  |  |
| Bearings | MP 5 | Y | Y | Y | Y |
| Side Lug | MS 2 |  | Y |  |  |
| Centre Line Lug | MS 3 |  |  |  |  |
| Side Tapped | MS 4 |  |  |  |  |
| Male Trunnion, Head | MT 1 | Y | Y | Y |  |
| Male Trunnion, Cap | MT 2 | Y | Y | Y |  |
| Male Trunnion, Central | MT 3 |  |  |  |  |
| Male Trunnion, Interm. | MT 4 | Y | Y | Y | Y |
| Tie Rods, Extended both ends | MX 1 |  | Y |  |  |
| Cap Studs / Tie Rods Extended | MX 2 |  | Y |  |  |
| Head Studs / Tie Rods Extended | MX 3 |  | Y |  |  |

For specific applications, Veljan offers Non-ISO type special mountings like Circular Flange at Head/ Cap, Square or Rectangular Flange at Head/Cap, Side flush mounting, etc.

|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |

## PISTON ROD

High tensile carbon steel, induction hardened to provide a dent-resistant surface, precision ground and hard chrome plated to extend bushing and seal life.

## ROD BUSH

High bearing strength phosphor Bronze rod guide of adequate bearing area.


## FLANGES

Machined steel flanges welded to tube to which end covers are bolted using high tensile fastners.

## PORTS

Larger size ports for higher speeds.

## BASIC DIMENSIONS

| BORE | ROD <br> ØMM | KK | A | EE <br> BSP | VE | WF | $\varnothing B$ | $\varnothing E$ | Y | PJ | ZJ | ZM |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 36 | M $27 \times 2.0$ | 36 | $1 / 2^{\prime \prime}$ | 29 | 47 | 63 | 108 | 95 | 125 | 240 | 315 |
| 63 | 45 | M $33 \times 2.0$ | 45 | $3 / 4^{\prime \prime}$ | 32 | 53 | 75 | 122 | 105 | 140 | 270 | 350 |
| 80 | 56 | M42X2.0 | 56 | $3 / 4^{\prime \prime}$ | 36 | 60 | 90 | 145 | 122 | 152 | 300 | 396 |
| 100 | 70 | $M 48 \times 2.0$ | 63 | $1^{\prime \prime}$ | 41 | 68 | 110 | 175 | 135 | 170 | 335 | 440 |
| 125 | 90 | $M 64 \times 3.0$ | 85 | $1^{\prime \prime}$ | 45 | 76 | 132 | 215 | 165 | 190 | 390 | 520 |
| 160 | 110 | $M 80 \times 3.0$ | 95 | $11 / 4^{\prime \prime}$ | 50 | 85 | 160 | 270 | 190 | 230 | 460 | 610 |
| 200 | 140 | M100X3.0 | 112 | $11 / 4^{\prime \prime}$ | 61 | 101 | 200 | 330 | 225 | 270 | 540 | 720 |
| 250 | 180 | M125X4 | 125 | $11 / 2^{\prime \prime}$ | 71 | 113 | 250 | 390 | 260 | 325 | 640 | 845 |
| 320 | 220 | $M 160 \times 4$ | 160 | $2^{\prime \prime}$ | 88 | 136 | 320 | 460 | 310 | 350 | 750 | 970 |


| BORE | VD <br> MIN | WC | FB | FC <br> Js 13 | NF | $\varnothing B$ <br> $\varnothing B A$ | $\varnothing U C$ | ZB <br> $M A X$ | ZP |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 4 | 22 | $8 \times \varnothing 13.5$ | 132 | 25 | 63 | 155 | 244 | 265 |
| 63 | 4 | 25 | $8 \times \varnothing 13.5$ | 150 | 28 | 75 | 175 | 274 | 298 |
| 80 | 4 | 28 | $8 \times \varnothing 17.5$ | 180 | 32 | 90 | 210 | 305 | 332 |
| 100 | 5 | 32 | $8 \times \varnothing 22$ | 212 | 36 | 110 | 250 | 340 | 371 |
| 125 | 5 | 36 | $8 \times \varnothing 22$ | 250 | 40 | 132 | 290 | 396 | 430 |
| 160 | 5 | 40 | $8 \times \varnothing 26$ | 315 | 45 | 160 | 360 | 467 | 505 |
| 200 | 5 | 45 | $8 \times \varnothing 33$ | 385 | 56 | 200 | 440 | 550 | 596 |
| 250 | 8 | 50 | $8 \times \varnothing 39$ | 475 | 63 | 250 | 540 | 652 | 703 |
| 320 | 8 | 56 | $8 \times \varnothing 45$ | 600 | 80 | 320 | 675 | 764 | 830 |



SINGLE ROD END


DOUBLE ROD END (NON ISO)


MF3: HEAD END CIRCULAR FLANGE MOUNTING


MF4 : CAP END CIRCULAR FLANGE MOUNTING


MP3: CAP FIXED EYE MOUNTING


MP5 : CAP FIXED EYE WITH SPHERICAL PLAIN BEARING MOUNTING

MT1: HEAD END TRUNNION MOUNTING


MT2 : CAP END TRUNNION MOUNTING


MT4 : INTERMEDIATE TRUNNION MOUNTING

| BORE | ØCD | ØCX | $\begin{gathered} \text { EX or EW } \\ M I N \end{gathered}$ | $\begin{aligned} & \text { L/LT } \\ & \text { MAX } \end{aligned}$ | MR/MS | XC/XO | Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 32 | 32 | 32 | 40 | 40 | 305 | $4^{0}$ |
| 63 | 40 | 40 | 40 | 50 | 50 | 348 |  |
| 80 | 50 | 50 | 50 | 63 | 63 | 395 |  |
| 100 | 63 | 63 | 63 | 71 | 71 | 442 |  |
| 125 | 80 | 80 | 80 | 90 | 90 | 520 |  |
| 160 | 100 | 100 | 100 | 112 | 112 | 617 |  |
| 200 | 125 | 125 | 125 | 160 | 160 | 756 |  |
| 250 | 160 | 160 | 160 | 200 | 200 | 903 |  |
| 320 | 200 | 200 | 200 | 250 | 250 | 1080 |  |





| TYPE | FORCE <br> NEWTONS | KK-THDS | CL | CE | CK | CM | LE | ER |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 20,000 | M16X1.5 | 45 | 52 | 20 | 20 | 27 | 25 |
| 25 | 32,000 | M20X1.5 | 56 | 65 | 25 | 25 | 34 | 32 |
| 32 | 50,000 | M27X2 | 70 | 80 | 32 | 32 | 42 | 40 |
| 40 | 80,000 | M33X2 | 90 | 97 | 40 | 40 | 52 | 50 |
| 50 | 125,000 | M42X2 | 110 | 120 | 50 | 50 | 64 | 63 |
| 63 | 200,000 | M48X2 | 140 | 140 | 63 | 63 | 75 | 71 |
| 80 | 320,000 | M64X3 | 170 | 180 | 80 | 80 | 94 | 90 |

ROD CLEVIS
(WITH PIVOT PIN)
(ISO : 8132-1986)


| TYPE | NOMINAL FORCE NEWTONS | $\begin{aligned} & \text { CK } \\ & \text { H9 } \end{aligned}$ | $\begin{gathered} \hline \mathrm{FL} \\ \mathrm{Js} 12 \end{gathered}$ | $\begin{gathered} \mathrm{LE} \\ \mathrm{MIN} \end{gathered}$ | $\begin{gathered} \mathrm{HB} \\ \mathrm{H} 13 \end{gathered}$ | $\begin{gathered} \text { MR } \\ \text { MAX } \end{gathered}$ | $\begin{gathered} \mathrm{CM} \\ \mathrm{~A} 12 \end{gathered}$ | $\begin{gathered} \mathrm{TB} \\ \mathrm{Js} 14 \end{gathered}$ | $\begin{gathered} \mathrm{CL} \\ \mathrm{~h} 16 \end{gathered}$ | $\begin{gathered} \mathrm{RC} \\ \mathrm{Js} 14 \end{gathered}$ | $\begin{aligned} & \text { UD } \\ & \text { MAX } \end{aligned}$ | $\begin{aligned} & \mathrm{UH} \\ & \text { MAX } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 20,000 | 20 | 45 | 30 | 11 | 20 | 20 | 75 | 45 | 32 | 58 | 98 |
| 25 | 32,000 | 25 | 55 | 37 | 13.5 | 25 | 25 | 85 | 56 | 40 | 70 | 113 |
| 32 | 50,000 | 32 | 65 | 43 | 17.5 | 32 | 32 | 110 | 70 | 50 | 85 | 143 |
| 40 | 80,000 | 40 | 76 | 52 | 22 | 40 | 40 | 130 | 90 | 65 | 108 | 170 |
| 50 | 125,000 | 50 | 95 | 65 | 26 | 50 | 50 | 170 | 110 | 80 | 130 | 220 |
| 63 | 200,000 | 63 | 112 | 75 | 33 | 63 | 63 | 210 | 140 | 100 | 160 | 270 |
| 80 | 320,000 | 80 | 140 | 95 | 39 | 80 | 80 | 250 | 170 | 125 | 210 | 320 |

CLEVIS BRACKET
(ISO : 8132-1986)

Note : These dimensions are valid for operation at 160 bar of cylinders with bore size of 40 mm (type 20) upto and including 160 mm (type 80); they are also valid for operation at 250 bar of cylinders with bore size of 50 mm (type 32) upto and including 125 mm (type 80).


ROD EYE
(ISO : 6981-1992)


ROD EYE WITH SPHERICAL BEARING (ISO : 6982-1992)

| TYPE | FORCE <br> NEWTONS | KK-THDS | AW | CA | CK | EM | c | b | A | UH | LE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 20,000 | M16X1.5 | 23 | 52 | 20 | 20 | 50 | 25 | 48 | 77 | 22 |
| 25 | 32,000 | M20X1.5 | 29 | 65 | 25 | 25 | 62 | 30 | 54 | 97 | 27 |
| 32 | 50,000 | M27X2 | 37 | 80 | 32 | 32 | 76 | 38 | 66 | 120 | 32 |
| 40 | 80,000 | M33X2 | 46 | 97 | 40 | 40 | 97 | 47 | 80 | 147 | 41 |
| 50 | 125,000 | M42X2 | 57 | 120 | 50 | 50 | 118 | 58 | 96 | 183 | 50 |
| 63 | 200,000 | M48X2 | 64 | 140 | 63 | 63 | 142 | 70 | 114 | 211 | 62 |
| 80 | 320,000 | M64X3 | 86 | 180 | 80 | 80 | 180 | 90 | 148 | 270 | 78 |
| 100 | 500,000 | M80X3 | 96 | 210 | 100 | 100 | 224 | 110 | 178 | 322 | 98 |
| 125 | 800,000 | M100X3 | 113 | 260 | 125 | 125 | 290 | 135 | 200 | 420 | 120 |
| 160 | 1250,000 | M125X4 | 126 | 310 | 160 | 160 | 340 | 165 | 250 | 510 | 150 |
| 200 | 2000,000 | M160X4 | 161 | 390 | 200 | 200 | 460 | 215 | 320 | 640 | 195 |

In the table below, we indicate the approximate weight of cylinder with zero stroke (Wo). W ${ }_{100}$ indicates the additional weight for each 100 mm stroke.

The weight of a cylinder $(W)$ with stroke length Smm is given by

$$
W=W_{o}+\frac{W_{100} S}{100} \mathrm{~kg}
$$

| $\begin{gathered} \text { BORE } \\ \mathrm{mm} \end{gathered}$ | $\begin{gathered} \mathrm{ROD} \\ \mathrm{~mm} \end{gathered}$ | SERIES 'HT' |  |  |  |  |  |  | SERIES 'HR' |  |  |  |  |  |  | SERIES 'HH' |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Wo in kg for various Mounting styles |  |  |  |  |  | $\begin{gathered} W_{100} \\ \mathrm{Kg} \end{gathered}$ | Wo in kg for various Mounting styles |  |  |  |  |  | $\begin{gathered} W_{100} \\ \mathrm{~kg} \end{gathered}$ | Wo in kg for various Mounting styles |  |  |  |  | $\begin{gathered} W_{100} \\ \mathrm{~kg} \end{gathered}$ |
|  |  |  <br> ME6 | MP1 <br>  <br> MP5 | MS2 | $\begin{gathered} \hline \text { MT1\& } \\ \text { MT2 } \end{gathered}$ | MT4 | $M X 1$, $M X 2 \&$ $M X 3$ |  | MF3 | MF4 | MP3\& MP5 | MS2 | $\begin{gathered} \text { MT1\& } \\ \text { MT2 } \end{gathered}$ | MT4 |  | MF3 | MF4 | $\begin{gathered} M P 3 \& \\ M P 5 \end{gathered}$ | $\begin{gathered} \hline \text { MT1\& } \\ \text { MT2 } \end{gathered}$ | MT4 |  |
| 40 | 18 | 4.7 | 4.2 | 4.0 | 3.9 | 4.6 | 3.7 | 0.9 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 22 |  |  |  |  |  |  |  | 6.7 | 7.0 | 6.2 | 6.5 | 5.8 | 6.7 | 1.0 |  |  |  |  |  |  |
|  | 28 | 4.9 | 4.4 | 4.2 | 4.1 | 4.8 | 3.9 | 1.2 | 6.8 | 7.1 | 6.3 | 6.6 | 5.9 | 6.8 | 1.2 |  |  |  |  |  |  |
| 50 | 22 | 7.2 | 7.0 | 6.5 | 6.3 | 7.9 | 5.9 | 1.4 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 28 |  |  |  |  |  |  |  | 11.0 | 11.6 | 10.2 | 10.9 | 9.5 | 10.8 | 1.6 |  |  |  |  |  |  |
|  | 36 | 7.6 | 7.4 | 6.9 | 6.7 | 3.3 | 6.3 | 1.8 | 11.2 | 11.8 | 10.4 | 11.1 | 9.7 | 11.0 | 1.8 | 15.6 | 16.6 | 15.4 | 13.9 | 15.9 | 1.9 |
| 63 | 28 | 10.2 | 10.1 | 9.7 | 3.9 | 10.6 | 8.5 | 1.9 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 36 |  |  |  |  |  |  |  | 17.7 | 19.0 | 16.7 | 18.5 | 15.5 | 17.0 | 2.2 |  |  |  | , |  |  |
|  | 45 | 10.9 | 10.8 | 10.4 | 9.6 | 11.3 | 9.2 | 2.7 | 18.0 | 19.3 | 17.0 | 18.8 | 15.8 | 17.3 | 2.7 | 21.1 | 22.6 | 21.7 | 18.9 | 21.8 | 2.7 |
| 80 | 36 | 18.9 | 19.5 | 17.3 | 16.5 | 20.5 | 16.0 | 2.7 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 45 |  |  |  |  |  |  |  | 26.6 | 28.6 | 25.6 | 26.2 | 22.8 | 24.9 | 3.0 |  | , |  |  |  |  |
|  | 56 | 20.0 | 20.6 | 13.4 | 17.6 | 21.5 | 17.1 | 3.9 | 27.3 | 29.3 | 26.3 | 26.9 | 23.5 | 25.6 | 3.6 | 38.2 | 40.7 | 40.6 | 34.9 | 39.4 | 4.2 |
| 100 | 45 | 25.0 | 28.0 | 24.0 | 22.7 | 26.0 | 22.0 | 4.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 56 |  |  |  |  |  |  |  | 46.6 | 49.3 | 46.8 | 49.7 | 41.5 | 45.8 | 4.5 |  |  |  |  |  |  |
|  | 70 | 26.9 | 29.7 | 25.9 | 24.6 | 27.5 | 23.9 | 5.8 | 47.3 | 50.0 | 47.5 | 50.5 | 42.2 | 46.5 | 5.8 | 59.5 | 63.5 | 62.9 | 54.9 | 63 | 6.2 |
| 125 | 56 | 48.0 | 53.0 | 44.0 | 43.0 | 48.0 | 42.0 | 6.5 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 70 |  |  |  |  |  |  |  | 75.1 | 79.3 | 78.5 | 81.1 | 69.8 | 78.6 | 7.2 |  |  |  |  |  |  |
|  | 90 | 51.7 | 65.7 | 47.7 | 46.7 | 51.7 | 45.7 | 9.5 | 78.0 | 82.2 | 81.4 | 84 | 727 | 81.5 | 9.5 | 106 | 112 | 118 | 101 | 116 | 9.8 |
| 160 | 70 | 78.0 | 90.0 | 73.0 | 71.0 | 84.0 | 69.0 | 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 90 |  |  |  |  |  |  |  | 125.7 | 133 | 137 | 139 | 119.5 | 131 | 11.5 |  |  |  |  |  |  |
|  | 110 | 83.0 | $95 . .0$ | 78.0 | 76.0 | 89.0 | 74.0 | 14 | 129.7 | 137 | 141 | 143 | 123.5 | 135 | 14 | 191 | 204 | 217 | 185 | 213 | 14.6 |
| 200 | 90 | 138 | 157 | 129 | 127 | 153 | 122 | 15 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 110 |  |  |  |  |  |  | 1 | 227 | 239 | 254 | 257 | 221 | 247 | 17 |  |  |  |  |  |  |
|  | 140 | 147 | 166 | 138 | 136 | 162 | 131 | 23 | 235 | 247 | 262 | 265 | 229 | 255 | 23 | 335 | 358 | 411 | 325 | 370 | 24 |
| 250 | 140 | 250 | 270 | 242 | 238 | 265 | 230 | 25 | 414 | 439 | 488 | 466 | 401 | 451 | 25 |  |  |  |  |  |  |
|  | 180 | 269 | 289 | 261 | 257 | 284 | 247 | 37 | 429 | 454 | 503 | 481 | 416 | 466 | 37 | 576 | 610 | 732 | 561 | 662 | 39 |
| 320 | 180 | 464 | 485 | 455 | 452 | 483 | 444 | 41 | 745 | 785 | 902 | 842 | 730 | 828 | 41 |  |  |  |  |  |  |
|  | 220 | 489 | 510 | 430 | 477 | 303 | 469 | 55 | 773 | 813 | 930 | 870 | 758 | 856 | 55 | 1016 | 1070 | 1312 | 975 | 1171 | 58 |

HOW TO ORDER VELJAN HYDRAULIC CYLINDERS

HT-Tie-rod type 160 bar compact series (ISO 6020-Part 2 \& Part 3)
HR-160 bar medium series (ISO 6020 Part1)
HH-250 bar series (ISO 6022)
*Note : Special requirements such as optional seals etc to be mentioned in text at the end of the ordering code.

